# United States Patent [19]

# Ryzin et al.

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[54]	GILL FOR EXTRACTING OXYGEN I	FROM
	OXYGEN BEARING FLUIDS	

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[56]

[22] Filed: Jul. 10, 1985

55/356; 114/334

58] Field of Search ...... 55/16, 158, 159, 356, 55/400; 114/67 R, 67 A, 334

## References Cited

## U.S. PATENT DOCUMENTS

	0.0. TATEM DOCUMENTS		
1,097,356	5/1914	Parnitzky	114/334
1,376,178	4/1921	Wagenseil	
1,412,073	4/1922	Wagenseil	
1,822,659	9/1931	Kirsch	
2,158,858	5/1939	Hoffmann	
2,434,453	1/1948	Beeman	
3,016,865	1/1962	Eichenberger	114/67 A
3,075,489	1/1963	Eichenberger	114/67 A
3,228,394	1/1966	Ayres	
3,333,583	8/1967	Bodell	128/200.2 S
3,369,343	2/1968	Robb	55/16
3,616,601	11/1971	Senkewich	114/334 X

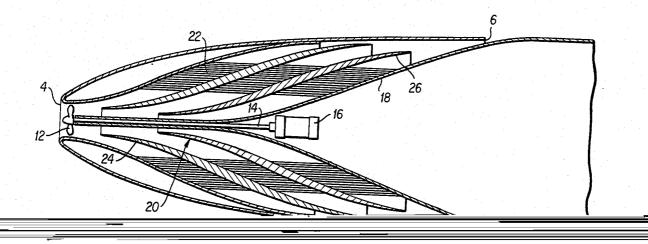
3,690,040	9/1972	Halfon 55/68 X
3,722,179	3/1973	Maen et al 55/68 X
3,910,780	10/1975	Henley et al 55/68 X
3,911,080	10/1975	Mehl et al 55/158 X
3,930,814	1/1976	Gessner 55/16
3,976,451	8/1976	Blackmer et al 55/158
3,979,190	9/1976	Hedman 55/158
4,174,955	11/1979	Blackmer et al 55/158
4,239,729	12/1980	Hasegawa et al 422/48
4,268,279	5/1981	Shindo et al 422/48 X
4,343,715	8/1982	Bonaventura et al 55/68 X
4,451,270	5/1984	Roman 55/68 X
4,537,606	8/1985	Itoh et al 55/158
4,542,010	9/1985	Roman et al 55/158 X
4,553,988	11/1985	Shimizu et al 55/158

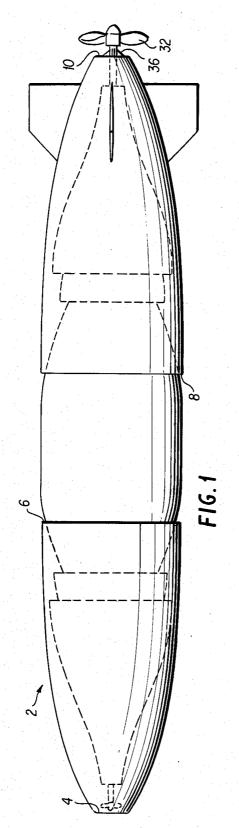
Primary Examiner—Robert Spitzer Attorney, Agent, or Firm—Oblon, Fisher, Spivak, McClelland & Maier

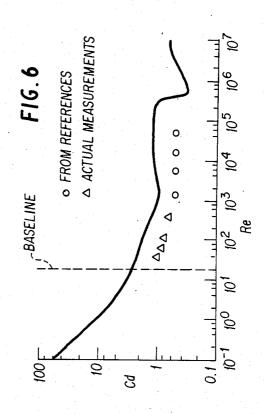
## [57] ABSTRACT

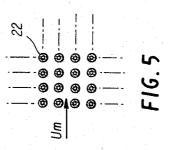
An apparatus for extracting oxygen from sea water in which a plurality of hollow gill members carry on oxygen extracting heme and are positioned within a diffuser. A flow of oxygen bearing liquid, such as sea water, passes through the diffuser and around the gill membranes. The gill membranes are angled with respect to the flow of sea water. The diffuser has a reduced section intake and outlet, and is divided into a number of channels, with the result that the drag force is reduced while maintaining adequate oxygen extraction. Propellers compensate for drag force losses.

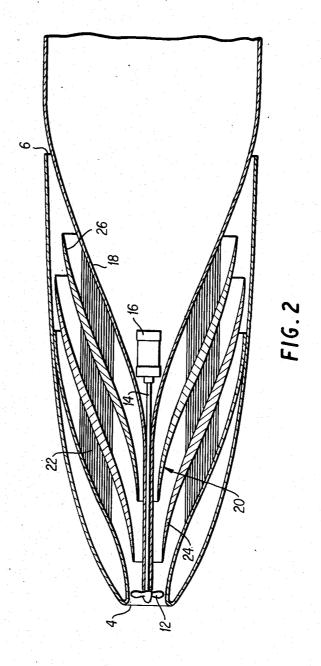
## 9 Claims, 6 Drawing Figures



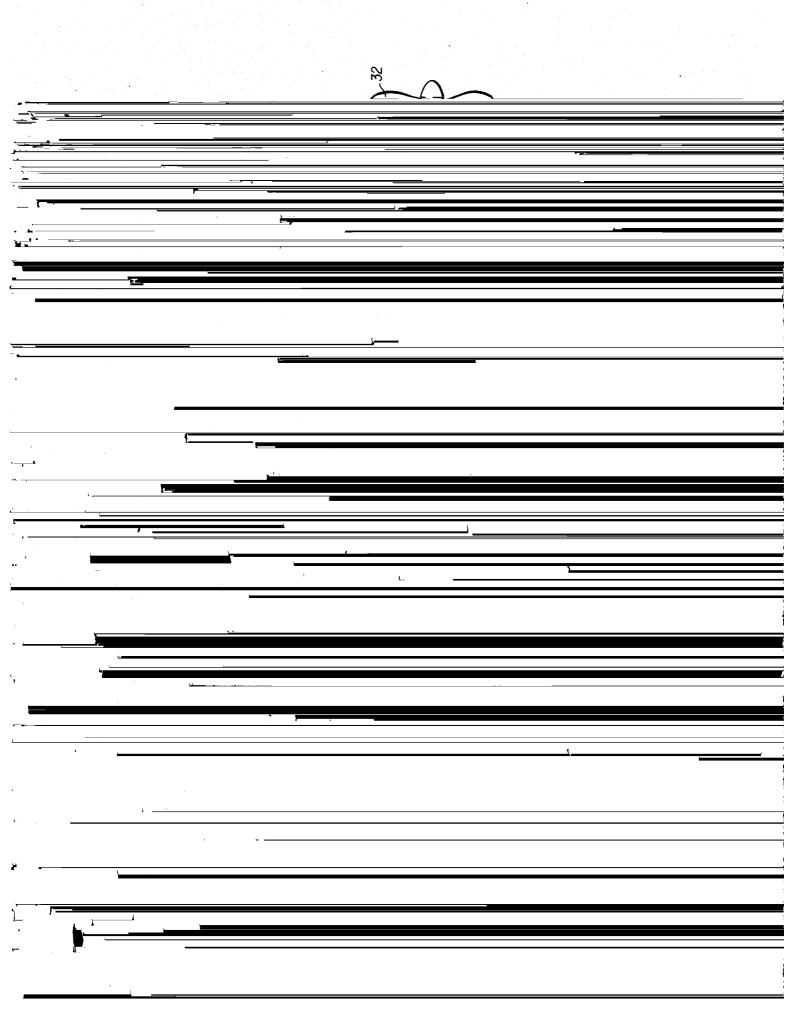


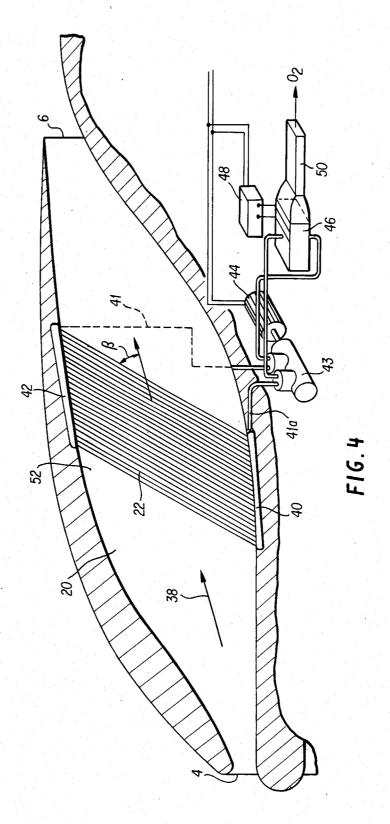






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# GILL FOR EXTRACTING OXYGEN FROM OXYGEN BEARING FLUIDS

## **BACKGROUND OF THE INVENTION**

1. Field of the Invention

This invention relates to a gill structure for extracting oxygen from fluids in which oxygen is dissolved.

2. Description of Related Art

Copending U.S. patent application Serial No. 10 653,850, filed on Sept. 24, 1984, now U.S. Pat. No. 4,602,987 and assigned to the same assignee as the present application, discloses a system and process for the extraction of oxygen from fluids in which oxygen is dissolved. This copending application is hereby incorporated by reference. The copending application discloses a process in which oxygen is extracted from an

velocity reduces the drag induced by the gill structure and increases the residence time of the sea water at the membranes.

The restrictions at the inlet and outlet of the diffuser will result in hydrodynamic resistance and a corresponding pressure drop thereacross. The present invention therefore provides a propelling means such as a propeller at the diffuser inlet or outlet which compensates for the hydrodynamic resistance of the membranes and other diffuser losses.

# BRIEF DESCRIPTION OF THE DRAWINGS

Various other objects, features and attendant advantages of the present invention will be more fully appreciated as the same becomes better understood from the following detailed description when considered in connection with the accompanying drawings in which like

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bow gill. The inlet 8 is annular and lacks a propeller. A main vehicle motor and controller 28, which may include a spark ignition internal combustion engine which consumes a portion of the oxygen produced by the gill structure, drives a drive shaft 30 and main vehicle pro- 5 peller 32. The shaft 30 is surrounded by an annular fairing 34, and is supported at the outlet 10 by a spyder 36. The motor and controller may be a well known internal combustion engine and controller therefor, and will not be described in detail.

The gill structure and heme supplying and circulating structure are schematically shown in FIG. 4, which only shows a single flow channel, and does not illustrate the propeller 12, for the sake of simplicity. The gill membranes 22 each consist of a hollow cylindrical tube 15 formed of a gas permeable material such as silicone rubber, polytetrafluoroethylene, an alkylcellulose or an acetylcellulose. The gills are arranged in an annular array of non-staggered rows as shown schematically in section in FIG. 5. The gills all extend radially and are 20 arranged at a uniform angle  $\beta$  with respect to the direction of flow 38 of the water from the intake.

Each end of each gill diaphragm is secured to an annular manifold 40 or 42 in a fluid tight manner, as by bonding using a waterproof resin. Heme or another 25 compound having similar oxygen absorbing and desorbing properties is circulated via lines 41a and 41b through the manifolds and gills by a pump 43, which is preferably a double piston pump for purposes of balance. The pump is driven by an electric motor 44, 30 which may be supplied with electrical power from a mator deison has the meeter 19. The he

ent for circular cylinder membrane bundles as a function of the Reynolds number, which is in turn is a function of the water velocity  $U_m$ . The base line refers to the minimum Reynolds number tested for. The solid line in the graph illustrates values of  $C_D$  for a single circular cylinder, the triangles represent actually measured values and the circles represent values derived from Grimson, E. D. "Correlation and Utilization of New Data on Flow Resistance and Heat Transfer for Cross Flow of Gases over Tube Banks," Trans, ASME 59, 583-594 (1937).

Accordingly, it can be appreciated that the gill structure reduces drag force attributable thereto in at least two ways. First, the relatively small diffuser intake area and outlet area result in a substantial reduction in the water velocity past the gill membranes. The resulting lowered Reynolds number results in a reduced value for the drag force which is proportional to the square of the fluid velocity.

A smaller angle  $\beta$  also produces reduced drag. However, as the angle  $\beta$  becomes smaller, the rate of oxygen extraction through the gill membranes is reduced since the gills present a smaller frontal area to the flow of oxygen bearing water. Increasing the number of gills will increase the rate of extraction, but will also increase the drag force. It has been found that an angle  $\beta = 25^{\circ}$ provides an optimum balance between these conflicting constraints of reducing drag while maintaining adequate oxygen extraction.

The propeller 12 within the bow gill replaces the anaman lant due to due a famou in the differen

extracted oxygen from the water passing through the diffuser 20, is pumped to an unloading chamber 46 having a power supply 48 and including a membrane 50,  $_{35}$ where the oxygen is extracted from the heme, by a process described in detail in the aforementioned copending U.S. patent application Ser. No. 653,850, now U.S. Pat. No. 4,602,987. The oxygen can then be used for various purposes, including for mixing with fuel for  $\eta_0$  where  $\eta =$  propellor efficiency

propeller 32 provides a similar function for the stern gill structure. The power Pprop supplied by the motor to each of the propellers 12 and 32 is based on the following equation

 $P_{prop} = \eta_{prop}(P_{dif} + P_{drag})$ 

- wherein an angle  $\beta$  formed between said flow direction and the longitudinal axes of said gills is less than 90°, whereby the drag force of said apparatus is reduced;
- wherein saidmeans for guiding comprise a diffuser 5 conduit having: an intake communicating with said source of liquid and having a first sectional area; a membrane supporting region in which said membranes are positioned, said membrane supporting said first sectional area; and an outlet communicating with said source of liquid downstream from said membrane supporting region in said flow direction, said outlet having a third sectional area small than said second section area; and
- wherein said means for providing relative movement comprises means in said intake or outlet for propelling liquid within said intake in said flow direction, whereby drag losses are compensated for.
- 2. The apparatus of claim 1, wherein  $\beta$  is less than 30°. 20
- 3. The apparatus of claim 1, wherein  $\beta$  is substantially 25°.

- 4. The apparatus of claim 1, wherein said membranes are arranged in an annular plurality of rows, all of said rows comprising membranes aligned with one another in said flow direction.
- 5. The apparatus of claim 1, wherein said membrane supporting region comprises a plurality of concentric annular membrane supporting regions arranged in parallel and separated by concentric annular fluid flow guide elements, each of said plurality of membrane region having a second sectional area larger than 10 supporting regions independently communicating with said inlet and said outlet.
  - 6. The apparatus of claim 1, including means for extracting said oxygen from said heme-like compound.
  - 7. The apparatus of claim 6, positioned at the up-15 stream end of an underwater vehicle in said flow direc-
    - 8. The apparatus of claim 6 positioned at both the upstream and downstream ends of said underwater vehicle.
    - 9. The apparatus of claim 8, wherein said vehicle includes vehicle propelling means.

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